BRUSHLESS D.C. DRIVE

FIELD OF THE INVENTION

The present invention is directed to a brushless d.c. drive.

BACKGROUND INFORMATION

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Brushless permanent-field d.c. drives may be used in motor vehicles for a variety of purposes, including electric power-assisted steering. These d.c. drives have a synchronous motor, which may have a star-connected stator winding or armature winding and a permanent-field rotor. The armature winding is connected to the direct voltage network by a converter in a bridge circuit having six semiconductor power breakers. The power inverter which causes commutation of the armature winding is controlled by an electronic controller. An example of a synchronous motor operated on a direct voltage network is discussed in German Published Patent Application No. 37 09 168.

If faults occur in the armature winding and/or in the power breakers, the d.c. drive may generate a permanent electromagnetic braking torque without a direct voltage being applied, if the synchronous motor operates as a generator against a low-resistance load impedance. In at least some applications, such a braking torque may have a negative effect on the functioning of the unit or system in which the d.c. drive is used. For example, in the case of electric power-assisted steering systems, the braking torque which occurs in the event of a fault may necessitate a considerable steering force being applied by the driver, which may be unacceptable. Accordingly, devices can be provided on such a d.c. drive to lead to a fail-silent response of the d.c. drive in the event

SUBSTITUTE SPECIFICATION

In an electric power-assisted steering system, a mechanical clutch, by way of which the output shaft of the synchronous motor acts on the steering gears, may be used to produce the desired fail-silent response. In the event of a fault, the clutch is opened to uncouple the motor from the steering system.

SUMMARY OF THE INVENTION

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The exemplary brushless d.c. drive according to the present invention may have the advantage that the desired fail-silent response of the d.c. drive is achieved without any expensive external components, such as mechanical clutches, with simple circuitry measures in the drive itself. Thus, the d.c. drive becomes more compact and requires less space, so that it can be used in a more versatile manner. The additional cost incurred for the desired response of the d.c. drive in the event of a fault may be greatly reduced.

According to an exemplary embodiment of the present invention, the separating apparatus, arrangement or structure for separating the connections between the winding phases of the armature winding may be activated by a control unit which detects a fault case.

According to another exemplary embodiment of the present invention, the control unit has, for this purpose, measurement shunts in each connecting line between the armature winding and the switching device designed as a bridge circuit having semiconductor switches. In simultaneous blocking phases of all semiconductor switches, the electric currents flowing through the measurement shunts are measured, and in the event of a

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current value which differs significantly from zero in one of the measurement shunts, the control device delivers an activation signal to the separating apparatus, arrangement or structure. Such a design of the control unit with which faults occurring in the switching device are detected may have the advantage that the measurement shunts already present in the d.c. drive for measuring the current for other reasons can also be used to detect the fault case, thus further reducing the complexity of the circuitry. Faults in the armature winding itself can be detected, for example, by measuring the braking torque delivered to the output shaft of the This may be an advantage in the case of synchronous motor. electric power-assisted steering systems, since sensors for measuring torques on the input and output shafts are already provided in the final control elements of the electric steering devices.

According to yet another exemplary embodiment of the present invention, the control unit in a star connection of the armature winding includes measurement shunts, each connecting a winding phase of the armature winding to the neutral point. The control unit continuously measures the amount and phase of currents flowing through the measurement shunts and adds the shunt currents as vectors. In the event of a significant deviation in the result of this addition from zero, the control unit delivers an activation signal to the separating means. With such a control unit, faults in the semiconductor switching device as well as faults in the armature winding may be detected, and the separating apparatus, arrangement or structure is activated accordingly.

According to other exemplary embodiments of the present invention, the separating apparatus, arrangement or structure may cause a reversible or irreversible separation of the connections between the winding phases of the armature

BRIEF DESCRIPTION OF THE DRAWINGS

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Figure 1 shows a circuit diagram of a brushless d.c. drive.

Figure 2 shows a circuit diagram of a modified armature winding of the d.c. drive in Figure 1.

Figure 3 shows a circuit diagram of the armature winding of the d.c. drive in Figure 1, having a modified control unit for controlling separating apparatus, arrangement or structure for separating the armature winding.

Figure 4 shows another exemplary embodiment of the circuit diagram of Figure 2.

Figure 5 shows another exemplary embodiment of the circuit diagram of Figure 2.

DETAILED DESCRIPTION

The brushless d.c. drive illustrated in Figure 1 includes a synchronous motor operated by a switching device 11 for electronic commutation on a direct voltage source 10. The synchronous motor, shown here with only its stator winding or armature winding 12, has a stator which holds armature winding 12 and a rotor which rotates in the stator and has permanent magnetic poles. Armature winding 12, which is designed in three phases, has three star-connected winding phases 13 in

the embodiment illustrated in Figure 1, their terminations 1, 2 and 3 being connected to switching device 11 by connecting line 14.

Switching device 11, designed as a B6 power inverter, has six semiconductor switches 15, which may be MOS-FETS, arranged in a bridge circuit. Connecting lines 14 leading to winding terminations 1, 2 and 3 are each connected to taps 4, 5 and 6 of a bridge branch formed by a series connection of two semiconductor switches 15, which is in the connection of two semiconductor switches 15. For commutation of armature winding 12, i.e., for applying winding phases 13 to direct voltage source 10 in the correct order, semiconductor switches 15 can be controlled by an electronic controller 16.

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The brushless d.c. drive has a device for forcing a failsilent response, which should ensure that in the event of a
fault in the d.c. drive, possibly caused by a defective
semiconductor switch 15 or by a winding termination in
armature winding 12, this does not interfere with or have a
negative effect on the system working with the d.c. drive.
This device includes separating apparatus, arrangement or
structure which, in the event of a fault, separate the
connections between winding phases 13 and a control unit 17,
which is integrated into controller 16 and, in the event of a
fault, detects the fault case and activates the separating
means. In the exemplary embodiment according to Figure 1,
three measurement shunts 18 belong to control unit 17, one
being connected to each of three connecting lines 14 between
switching device 11 and armature winding 12.

In time intervals during which all semiconductor switches 15 are blocked, control unit 17 measures the shunt currents flowing over measurement shunts 18. If all semiconductor switches 15 are intact, each shunt current is zero. If control

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In the embodiment according to Figure 1, the separating apparatus, arrangement or structure acts on neutral point 20 of armature winding 12, causing an irreversible separation of the neutral point connection of winding phases 13 when activated. The separating apparatus, arrangement or structure may be, for example, a pyrotechnic blasting capsule 19, such as that used in motor vehicles to deploy airbags in the event of a crash. Electrically ignitable blasting capsule 19 is connected first to control unit 17 by way of a connecting line 40 and second to the negative potential of direct voltage source 10. If one of measurement shunts 18 delivers a current value differing significantly from zero, control unit 17 generates an electric firing pulse which ignites blasting capsule 19. The exploding blasting charge ruptures neutral point 20, thus separating winding phases 13 from one another. In this way, the in-system d.c. drive, which is driven by the system by way of its output shaft in the event of a fault, cannot generate a braking torque because separated armature winding 12 does not allow generator operation.

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With control unit 17 described in conjunction with Figure 1, only faults based on defects in semiconductor switches 15 can be detected. To also detect possible faults occurring in armature winding 12, control unit 17 according to Figure 3 is modified so that measurement shunts 18 present in feeder lines 14 are eliminated, and, instead, measurement shunts 21 are arranged between neutral point 20 and each winding phase 13. Control unit 17 measures the amount and phase of electric currents flowing over measurement shunts 21 and adds them as vectors. In a fault-free d.c. motor, the result of this

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relays, for example.

Armature winding 12 of the synchronous motor may also be connected in a delta connection, for example, as illustrated in the circuit diagram in Figure 2. Winding phases 13 are connected to winding terminations 1, 2 and 3. The separating apparatus, arrangement or structure for separating winding phases 13 in the event of a fault is integrated into winding phases 13 and connected in series with them. In the exemplary 20<u>]</u> embodiment in Figure 2, the response of the separating apparatus, arrangement or structure causes a reversible separation of armature winding 12. To achieve the reversible separation, an electric switching contact 23, which may be controlled by an electronic or mechanical apparatus, arrangement or structure, is arranged between winding terminations 1, 2 and 3 and winding phases 13. Electronically controllable switching contacts 23 are implemented by

transistors or thyristors, for example, and mechanically controllable switching contacts 23 may be electromagnetic

In the exemplary embodiment in Figure 4, like the exemplary embodiment according to Figure 1, the separating apparatus, arrangement or structure are arranged at neutral point 20 of armature winding 12. When activated, the separating apparatus,

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arrangement or structure causes an irreversible separation of neutral point 20. The separating apparatus, arrangement or structure includes two switching contacts 25 which are preloaded in the direction of opening and are each held in the closed position by a holding element 26. A switching contact 25 having a holding element 26 is arranged between neutral point 20 and the end of the winding of each of two winding phases 13. It is not necessary to provide a third switching contact having a holding element between neutral point 20 and third winding phase 13. A common electrically ignitable pyrotechnic blasting capsule 27 is provided for both holding elements 26 and is capable of destroying both holding elements 26 when deployed. As in the exemplary embodiment according to Figure 1, blasting capsule 27 is connected by connecting line 40 to control unit 17 which applies an electric firing pulse to blasting capsule 27 in the event of a fault. With destruction of holding elements 26, prestressed switching contacts 25 are released and opened, so that the connection of two winding phases 13 to neutral point 20 is interrupted suddenly.

Figure 4 illustrates a structural embodiment for two switching contacts 25 which are prestressed in the direction of opening and have a holding element 26 and a common blasting capsule 27 for holding elements 26. Each switching contact 25 has a contact plate 28 fixedly connected to an operating pin 29. Axially displaceable operating pin 29 is loaded by a compression spring 30 which is supported on a spring plate 31 connected to operating pin 29 and on a stationary stop 32 and prestresses operating pin 29 so that contact plate 28 is lifted up from contact points 33, 34. Both holding elements 26 have a common lock block 35 in which both operating pins 29 engage, each with a locking projection 36 provided on its end which faces away from contact plate 28. When ignited, blasting capsule 27, which is arranged inside lock block 35, destroys

lock block 35. In assembly, switching contacts 25 are closed by pressing contact plate 28 against contact points 33, 34 with tensioning of compression springs 30, so that locking projection 36 falls into lock block 35 and is held in place. In the case of a fault, blasting capsule 27 is ignited by control unit 17. This destroys lock block 35, thus releasing operating pins 29, and prestressed compression springs 30 lift contact plates 28 away from contact points 33, 34.

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In the exemplary embodiment according to Figure 5, as in the 10 exemplary embodiment according to Figure 2, armature winding C] 12 is connected in a delta connection. It is necessary in this 4I * # # 15 # # 15 # # exemplary embodiment for each branch of the delta connection to be separated in the event of a fault, so that a switching contact 25 having a holding element 26 is connected to each winding phase 13 in series. In exemplary Figure 5, a separate blasting capsule 27 is provided for each holding element 26, J destroying holding element 26 when deployed, so that switching contact 25 which is prestressed in the closing direction opens automatically. A common blasting capsule 27 may also be used 201 to destroy all three holding elements 26. Prestressed switching contacts 25 having holding element 26 may be as described in conjunction with Figure 4. In the switching contacts 25 as prestressed spring tongues, separate compression springs 30 for opening switching contacts 25 may 25 be omitted.

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